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3 **Development and Evaluation of a**

4 **Hydrostatic Dynamical Core using the Spectral**

5 **element/Discontinuous Galerkin Methods**

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Abstract

In this paper, we present a dynamical core for the atmospheric primitive hydrostatic equations using a unified formulation of spectral element (SE) and discontinuous Galerkin (DG) methods in the horizontal direction with a finite difference (FD) method in the radial direction. The CG and DG horizontal discretization employs high-order nodal basis functions associated with Lagrange polynomials based on Gauss-Lobatto-Legendre (GLL) quadrature points, which define the common machinery. The atmospheric primitive hydrostatic equations are solved on the cubed-sphere grid using the flux form governing equations in a three-dimensional (3D) Cartesian space. By using Cartesian space, we can avoid the pole singularity problem due to spherical coordinates and this also allows us to use any quadrilateral-based grid naturally. In order to consider an easy way for coupling the dynamics with existing physics packages, we use a FD in the radial direction. The models are verified by conducting conventional benchmark test cases: the Rossby-Haurwitz wavenumber 4, Jablonowski-Williamson tests for balanced initial state and baroclinic instability, and Held-Suarez tests. The results from those tests demonstrate that the present dynamical core can produce numerical solutions of good quality comparable to other models..

1. Introduction

Spectral element (SE; here after is referred to as continuous Galerkin (CG)) and discontinuous Galerkin (DG) methods are very attractive on many-core computing platforms because these methods decompose the physical domain into smaller pieces having a small communication footprint. CG/DG methods are local in nature and thus can have a large on-processor operation count (Kelly and Giraldo, 2012) which is advantageous on large processor-count computers. Also CG/DG methods can achieve high-order accuracy because the polynomial order can be adjusted automatically according to the corresponding numerical integration rule, that is, the Gaussian quadrature (Taylor et al. 1997; Giraldo 2001; Giraldo et al. 2002). In addition, CG/DG methods are geometrically flexible in the types of grids they can use; this includes static and adaptive grids as well as conforming and non-conforming grids (Giraldo et al. 2002; Giraldo and Rosmond 2004; Mueller et al. 2013).

The CG method is characterized by the high-order approximation combined with the local decomposition property of the finite element method (FEM) and weak numerical dispersion property of the spectral method. The DG method, on the other hand, is best characterized as a combination of the properties of the CG method plus the local conservation properties of the finite volume method (FVM) (Giraldo and Restelli 2008). The virtues of the DG method are that it is inherently conservative (both locally and globally) as in the case of the FVM. However, the common criticism of the DG method is the stringent Courant-Friedrichs-Lewy (CFL) stability constraint in explicit time schemes. For a DG method using k -th order basis functions, an approximate CFL limit estimate is $1/(2k+1)$ (Cockburn and Shu 1989). This, however, is partly due to the choice of the numerical flux which, for expediency, is chosen as a purely edge-based flux although other fluxes are also possible (e.g., Yelash et al. 2014); however these more sophisticated approaches come at a price and it is yet unclear

which strategy yields a faster wallclock time to solution.

To date, successful applications of the CG method in hydrostatic atmospheric modeling include the Community Atmosphere Model – spectral element dynamical core (CAM-SE) (Dennis et al. 2012) and the scalable spectral element Eulerian atmospheric model (NSEAM) (Giraldo and Rosmond, 2004, hereafter GR04). In this context, one of the motivations of this study is to construct a dynamical core using a unified formulation of CG and DG methods as described in Giraldo and Restelli 2008 and Kelly and Giraldo 2012 where nonhydrostatic atmospheric models are proposed. Successful applications of the DG method in hydrostatic atmospheric modeling include the work of Nair et al. 2009; however, in our paper we shall present results for more than one test case. To our knowledge, the results for the Held-Suarez test cases presented in our paper are the first such results shown for a DG model. The significance is that this confirms the long-term stability of the DG method for hydrostatic models. Although we could also discretize the vertical direction with CG and DG methods, we choose a conservative flux-form finite-difference method for discretization in the vertical direction which is similar to the approach used in both CAM-SE and NSEAM. This choice of vertical discretization provides an easy way for coupling the dynamics with existing physics packages.

In this paper we construct a unified formulation of CG and DG for the primitive hydrostatic equations in GR04. In order to achieve a unified formulation, the advective-form governing equations in GR04 are recast in flux form. GR04 provides a clue for converting the advective-form equation set in 3D Cartesian space to the flux form in their appendix. By using 3D Cartesian space, we can be free from the pole singularity problem in spherical coordinates. Although a local Cartesian coordinate system could also be used to overcome these problems (Taylor et al. 1997; Nair et al. 2005), the use of 3D Cartesian space everywhere allows us to treat the pole as any other point. Therefore it permits general grids

naturally such as icosahedral, hexahedral, and adaptive unstructured grids (it should be noted that general grids can also be used with the coordinate invariant form of the equations). In this paper we adopt a hexahedral grid – the so called cubed-sphere.

In brief, the objective of this paper is to show the feasibility of the hydrostatic primitive equation models using CG/DG horizontal discretization and the FD vertical discretization by conducting conventional benchmark test cases. The organization of the remainder of this paper is as follows. In the next section we describe the governing equations in 3D Cartesian space with a definition of the prognostic and diagnostic variables. In Sec. 3 we explain the horizontal, vertical, and temporal discretization methods including the numerical approximation of the equations. In Sec. 4 we describe the cubed-sphere grid, and in Sec. 5, we present the simulation results of the test cases. Finally, in Sec. 6, we end the paper with a summary of our findings and some concluding remarks.

2. Governing Equations

The primitive hydrostatic equations of conservation form in the 3D Cartesian space with a sigma pressure vertical coordinate σ are given as

$$\frac{\partial q}{\partial t} + \nabla \cdot \bar{F} = S_{Cor} + S_h + S_v, \quad (1)$$

where

$$q = \begin{bmatrix} \pi \\ U \\ V \\ W \\ \Theta \end{bmatrix} = \begin{bmatrix} \pi \\ \pi U \\ \pi V \\ \pi W \\ \pi \theta \end{bmatrix} \quad (2)$$

are prognostic variables,

$$\begin{aligned}
111 \quad S_{Cor} &= \begin{bmatrix} 0 \\ -\frac{2\omega Z}{a^2}(yW - zV) - \mu x \\ -\frac{2\omega Z}{a^2}(zU - xW) - \mu y \\ -\frac{2\omega Z}{a^2}(xV - yU) - \mu z \\ 0 \end{bmatrix}, \quad S_h = \begin{bmatrix} 0 \\ (\phi - \Theta C_p \frac{\partial P}{\partial \pi}) \frac{\partial \pi}{\partial x} \\ (\phi - \Theta C_p \frac{\partial P}{\partial \pi}) \frac{\partial \pi}{\partial y} \\ (\phi - \Theta C_p \frac{\partial P}{\partial \pi}) \frac{\partial \pi}{\partial z} \\ 0 \end{bmatrix}, \quad S_v = \begin{bmatrix} -\frac{\partial}{\partial \sigma}(\pi \dot{\sigma}) \\ -\frac{\partial}{\partial \sigma}(U \dot{\sigma}) \\ -\frac{\partial}{\partial \sigma}(V \dot{\sigma}) \\ -\frac{\partial}{\partial \sigma}(W \dot{\sigma}) \\ -\frac{\partial}{\partial \sigma}(\Theta \dot{\sigma}) \end{bmatrix} \quad (3)
\end{aligned}$$

112 respectively denote Coriolis with the Lagrange multiplier μ , horizontal, and vertical source
 113 terms, and

$$\begin{aligned}
114 \quad \bar{\mathbf{F}} &= \begin{bmatrix} U \\ \frac{U^2}{\pi} + \pi\phi \\ \frac{VU}{\pi} \\ \frac{WU}{\pi} \\ \frac{\Theta U}{\pi} \end{bmatrix} \hat{i} + \begin{bmatrix} V \\ \frac{UV}{\pi} \\ \frac{V^2}{\pi} + \pi\phi \\ \frac{WV}{\pi} \\ \frac{\Theta V}{\pi} \end{bmatrix} \hat{j} + \begin{bmatrix} W \\ \frac{UW}{\pi} \\ \frac{VW}{\pi} \\ \frac{W^2}{\pi} + \pi\phi \\ \frac{\Theta W}{\pi} \end{bmatrix} \hat{k} \quad (4)
\end{aligned}$$

115 is the horizontal flux terms where \hat{i} , \hat{j} , and \hat{k} denote the Cartesian directional unit
 116 vectors. The prognostic variables q are comprised of: 1) the surface pressure π defined as

$$117 \quad \pi = p_s - p_t, \quad (5)$$

118 where p_s is the true surface pressure, and p_t is the pressure at the top of the atmosphere; 2)

119 the flux-form velocity components $\mathbf{U} = (U, V, W) = (\pi u, \pi v, \pi w)$, where (u, v, w) are the

120 three Cartesian velocity components, and 3) the flux-form potential temperature $\Theta = \pi\theta$,

121 where θ is the potential temperature. The diagnostic variables are 1) the geopotential ϕ

122 given by the diagnostic equation as

$$\frac{\partial \phi}{\partial P} = -c_p \theta, \quad (6)$$

2) the Exner function P defined as

$$P = \left(\frac{p}{p_0} \right)^{R_d / c_p}, \quad (7)$$

where p and p_0 is the hydrostatic pressure and standard surface pressure, respectively,

and R_d and c_p is the gas constant and specific heat of dry air at constant pressure, and 3)

the σ -coordinate vertical velocity $\omega = \frac{d\sigma}{dt}$ where $\sigma = \frac{p - p_t}{\pi} \in [0, 1]$ is the definition

of the sigma pressure coordinate with a value of 0 at the top of the atmosphere and 1 at the

surface. The constants a and ω in Eq. (4) are the Earth's radius and angular velocity,

respectively, and μ is a Lagrange multiplier for the fluid particles to remain on a spherical

shell with constant σ . The momentum variables representing the atmospheric motion over

the shell in the Cartesian space have three components along the x, y, and z axes in Cartesian

coordinates, so that the movement of a particle on the shell has three degrees of freedom,

which can move freely in \mathbb{R}^3 . To ensure that fluid particles remain on the spherical shell, it is

required that the fluid velocity remains perpendicular to the position vector, which yields a

Lagrange multiplier in the momentum equations (Giraldo 2001; Giraldo et al. 2002; Giraldo

and Rosmond, 2004). It is noteworthy that among the independent variables (x, y, z, σ, t) ,

(x, y, z) represent grid points on the sphere which are related to the points in the spherical

coordinates (λ, φ) given as

$$\begin{aligned} x &= a \cos \lambda \cos \varphi, \\ y &= a \sin \lambda \cos \varphi, \\ z &= a \sin \varphi. \end{aligned} \quad (8)$$

Thus ∇ is defined as

$$\nabla = \begin{pmatrix} \frac{\partial}{\partial x} \\ \frac{\partial}{\partial y} \\ \frac{\partial}{\partial z} \end{pmatrix} \quad (9)$$

at constant σ .

3. Discretization

1) Discretization in the horizontal direction

To describe the discretization of the horizontal operators by the CG/DG method we follow the description given previously in Giraldo and Restelli 2008 and in Kelly and Giraldo 2012. Let us begin by rewriting Eq. (1) as follows

$$\frac{\partial q}{\partial t} + \nabla \cdot F = S \quad (10)$$

Next, let us introduce the following vector spaces

$$V^{CG} = \left\{ \psi \in H^1(\Omega) \mid \psi \in P_N(\Omega_e) \right\} \quad (11)$$

and

$$V^{DG} = \left\{ \psi \in L^2(\Omega) \mid \psi \in P_N(\Omega_e) \right\} \quad (12)$$

where we now seek solutions of Eq. (1) as follows:

$$q \in V \quad \forall \psi \in V$$

where V denotes either V^{CG} or V^{DG} . Next, we approximate the solution vector as follows

$$q_N(x, y, z, t) = \sum_{i=1}^M \psi_i(x, y, z) q_i(t) \quad (13)$$

where, for quadrilateral elements in the horizontal direction, $M = (N + 1)^2$ with N

representing the polynomial order of the basis function ψ .

We now introduce this expansion into our governing system of equations, multiply by a test function, and integrate by parts to yield

$$\int_{\Omega_e} \psi_i \frac{\partial q_N}{\partial t} d\Omega_e + \int_{\Gamma_e} \psi_i \hat{n} \cdot F d\Gamma_e - \int_{\Omega_e} \nabla \psi_i F(q_N) d\Omega_e = \int_{\Omega_e} \psi_i S(q_N) d\Omega_e. \quad (14)$$

where the terms with Ω_e refer to volume integrals and the one with Γ_e is a boundary integral which accounts for both internal faces (neighboring elements share faces) as well as boundary faces (elements on boundaries do not share faces with other elements). In matrix-vector form, this equation can be written as

$$M_{i,j}^e \frac{dq_j^e}{dt} + (\mathbf{M}_{i,j}^{F,e})^T F_j^*(q_N) - (\mathbf{D}_{i,j}^e)^T F_j(q_N^e) = S_i(q_N^e) \quad (15)$$

where

$$\begin{aligned} M_{i,j}^e &= \int_{\Omega_e} \psi_i \psi_j d\Omega_e, \\ \mathbf{M}_{i,j}^{F,e} &= \int_{\Gamma_e} \psi_i \psi_j \hat{n} d\Gamma_e, \\ \mathbf{D}_{i,j}^e &= \int_{\Omega_e} \nabla \psi_i \psi_j d\Omega_e. \end{aligned} \quad (16)$$

These matrices represent: the mass, flux, and differentiation matrices, respectively.

For the DG method, the matrix-vector form given above is sufficient as long as we define the numerical flux, e.g., as follows

$$F^*(q_N) = \frac{1}{2} \left[F(q_N^L) + F(q_N^R) - \hat{n} |\lambda_{\max}| (q_N^R - q_N^L) \right] \quad (17)$$

where the superscripts L and R refer to the left and right elements (arbitrarily decided) of the face Γ_e and λ_{\max} is the maximum eigenvalue of the Jacobian matrix of the governing partial differential equations. Here we use the Rusanov scheme for the numerical flux because of its simplicity although any other Riemann solver could be used. For the CG method, the matrix-vector form given above is also used except that the term of the flux

matrix vanishes on the sphere and we then use the direct stiffness summation (DSS) operation which gathers the element-wise solution to a global grid point solution and then scatters it back to the element-wise space. This is done to ensure that the solution is C^0 across all element faces.

2) Discretization in the vertical direction

We use the FD method similarly to other global models to gain an easy way for coupling the dynamics with existing physics packages, although we could also discretize the vertical operators with the CG/DG methods (as done in Kelly and Giraldo 2012; Giraldo et al. 2013). Also by using the FD, we can keep the model as similar as possible to the NSEAM model (GR04) so that we directly discern differences from the discrete horizontal operators. Using a Lorenz staggering, the variables U , V , W , Θ , and ϕ are at layer mid points denoted by $k = 1, 2, \dots, Nlev$ where $Nlev$ is the total number of layers, while the variable P and \mathcal{E} are at layer interface points denoted by $k + \frac{1}{2}$, $k = 0, 1, \dots, Nlev$.

We begin the vertical discretization by the evaluating $\frac{\partial \pi}{\partial t}$ which is given by integrating the first row of Eq. (1) (i.e., the continuity equation) from the surface ($\sigma_{bottom} = \sigma_{Nlev+1/2} = 1$) to the top ($\sigma_{top} = \sigma_{1/2} = 0$) with no-flux boundaries at the top and bottom levels of the atmosphere (i.e. $\mathcal{E}_{top} = \mathcal{E}_{bottom} = 0$). Thus,

$$\frac{\partial \pi}{\partial t} = \mathbf{M}^{-1} \sum_{k=1}^{Nlev} \mathbf{D}_k^T \mathbf{U}_k \Delta \sigma_k, \quad (18)$$

where k is the number of vertical levels to be integrated across and $\Delta \sigma_l = \sigma_{l+1/2} - \sigma_{l-1/2}$ is the thickness of the layer. Then the vertical velocity \mathcal{E} at each vertical level is obtained by integrating the continuity equation from the top of the atmosphere to the material surface as

203 follows

$$204 \quad (\dot{\sigma}\pi)_{k+1/2} = -\frac{\partial\pi}{\partial t}\sigma_{k+1/2} + \mathbf{M}^{-1}\sum_{l=1}^k \dot{\mathbf{D}} \cdot \mathbf{U}_l \Delta\sigma_l. \quad (19)$$

205 The vertical advection term $\frac{\partial(\dot{\sigma}q)}{\partial\sigma}$ in the vertical source term S_v is computed using the
 206 third-order upwind biased discretization in Hundsdorfer et al. (1995) which is given as

$$207 \quad \left. \frac{\partial f}{\partial\sigma} \right|_k = \frac{f_{k-2} - 8f_{k-1} + 8f_{k+1} - f_{k+2}}{12\Delta\sigma} + \text{sign}(q) \frac{f_{k-2} - 4f_{k-1} + 6f_k - 4f_{k+1} + f_{k+2}}{12\Delta\sigma}, \quad (20)$$

208 where f denotes the flux (q). It is noted that the upwind-biased schemes are inherently
 209 diffusive. Following GR04, the hydrostatic equation, Eq. (6), is evaluated as follows

$$210 \quad \phi_k - \phi_{k+1} = c_p \Theta_k (P_{k+1/2} - P_k) + c_p \Theta_{k+1} (P_{k+1} - P_{k+1/2}), \quad (21)$$

211 where the Exner function at layer interfaces and midpoints is given by

$$212 \quad P_{k+1/2} = \left(\frac{p_{k+1/2}}{p_0} \right)^\kappa \quad (22)$$

213 and

$$214 \quad P_k = \frac{1}{\kappa+1} \frac{1}{p_0^\kappa} \left(\frac{p_{k+1/2}^{\kappa+1} - p_{k-1/2}^{\kappa+1}}{p_{k+1/2} - p_{k-1/2}} \right), \quad (23)$$

215 respectively.

216

217 3) Discretization in time

218 For integrating the equations, we adopt a third-order strong stability preserving explicit
 219 Runge-Kutta (SSP-RK) scheme (Cockburn and Shu 1998; Nair et al. 2005). The 3rd order
 220 SSP-RK scheme is introduced into our governing equations in the form of

$$221 \quad \frac{\partial q}{\partial t} = R(q), \quad (24)$$

222 and is given as follows:

$$\begin{aligned}
 q^{(1)} &= q^n + \Delta t R(q^n) \\
 q^{(2)} &= \frac{3}{4}q^n + \frac{1}{4}q^{(1)} + \frac{1}{4}\Delta t R(q^{(1)}) \\
 q^{n+1} &= \frac{1}{3}q^n + \frac{2}{3}q^{(1)} + \frac{2}{3}\Delta t R(q^{(2)}),
 \end{aligned} \tag{25}$$

224 where the superscripts n and $n+1$ denote time levels t and $t + \Delta t$, respectively. While
 225 for smooth problems the SSP-RK scheme does not generate spurious oscillations so that are
 226 widely used for DG methods, for problems with strong shocks or discontinuities, oscillations
 227 can lead to nonlinear instabilities (Cockburn and Shu 1998). Since an SSP-RK time-
 228 integration scheme cannot control such undesirable effects, a Boyd-Vandeven spatial filter is
 229 applied after the time integration, which is described in GR04. Neither viscosity nor slope
 230 limiter are used in all simulations.

231

232 4. Cubed-sphere Grid

233 The cubed-sphere grids are composed of the six patches obtained by the gnomonic
 234 projection of the faces of the hexahedron which are subdivided into $(n_H \times n_H)$ quadrilateral
 235 elements where n_H is the number of quadrilateral elements in each direction (GR04). Inside
 236 each element we build $(N + 1)$ Gauss-Lobatto-Legendre (GLL) quadrature points, where N
 237 indicate the polynomial order of the basis function ψ . Therefore the total number of grid
 238 points N_p is given as

$$N_p = 6(n_H N)^2 + 2, \tag{26}$$

240 and the number of elements N_e comprising the sphere is

$$N_e = 6(n_H)^2. \tag{27}$$

241

242 We now introduce the square region on the gnomonic space $(\xi_G, \eta_G) = \left[-\frac{\pi}{4}, +\frac{\pi}{4}\right]^2$ in
 243 each of the six faces to describe the relation to spherical coordinates (λ, φ) . The gnomonic
 244 space $(\xi_G, \eta_G) = \left[-\frac{\pi}{4}, +\frac{\pi}{4}\right]^2$ is mapped to the corresponding spherical coordinates
 245 (λ_G, φ_G) via

$$246 \quad \lambda_G = \xi_G, \quad (28)$$

$$247 \quad \varphi_G = \arcsin \left(\frac{\tan \eta_G}{\sqrt{1 + \tan^2 \xi_G + \tan^2 \eta_G}} \right), \quad (29)$$

248 and then we construct the cubed-sphere grid by rotating this face to the six faces of the
 249 hexahedron by

$$250 \quad \lambda = \lambda_c + \arctan \left(\frac{\cos \varphi_G \sin \lambda_G}{\cos \varphi_G \cos \lambda_G \cos \varphi_c - \sin \varphi_G \sin \varphi_c} \right), \quad (30)$$

$$251 \quad \varphi = \arcsin (\sin \varphi_G \cos \varphi_c + \cos \varphi_G \cos \lambda_G \sin \varphi_c), \quad (31)$$

252 with the centroids, $(\lambda_c, \varphi_c) = \left(\left[c - 1 \right] \frac{\pi}{2}, 0 \right)$ for $c = 1, 2, 3, 4, 5, 6$, $(\lambda_5, \varphi_5) = \left(0, \frac{\pi}{2} \right)$, and
 253 $(\lambda_6, \varphi_6) = \left(0, -\frac{\pi}{2} \right)$.

254 The resolution of the cubed-sphere grid H is determined by n_H (the number of
 255 quadrilateral elements in each direction contained in each of the six faces of the cube) and N
 256 (the polynomial order of the elements), where we use $H = n_H N$ as the convention to define
 257 the grid resolution. Fig. 1 show examples of the grids with $H = 3$ ($n_H = 3$ and $N = 1$),
 258 $H = 15$ ($n_H = 3$ and $N = 5$), and $H = 35$ ($n_H = 5$ and $N = 7$).

5. Simulation results with Benchmark Tests

We consider the following test cases: 1) 3D Rossby-Haurwitz wavenumber 4, 2) Jablonowski-Williamson balanced initial state test, 3) baroclinic instability test, and 4) Held-Suarez test. Because all of the test cases except 2) the Jablonowski-Williamson balanced initial state test do not have analytical solutions, we compare our results to the results of other published papers and evaluate the results qualitatively. We now discuss the results of the four test cases.

1) 3D Rossby-Haurwitz wavenumber 4

We conduct the Rossby-Haurwitz (RH) wave test case which is a 3D extension of the 2D shallow water RH wave discussed in Williamson et al. (1992). The main differences compared to the 2D shallow water formulation include the introduction of a temperature field and the derivation of the surface pressure, which is discussed in GR04 and Jablonowski et al. (2008). The Rossby-Haurwitz wave approximately preserves its shape even in nonlinear shallow water and primitive equation models, which has a sufficiently simple enough pattern to allow one to judge if the simulation was successful. We initialize the model following Jablonowski et al. (2008).

Snapshots of the output data for the CG and DG models for day 15 are presented in Figs. 2 and 3, respectively. The figures show the 850 hPa zonal wind, meridional wind, and temperature as well as the surface pressure. These model results were computed at the resolution of $H = 64$ ($n_H = 8$ and $N = 8$) with 26 vertical levels (Nlev=26). The results of the CG and DG simulations are virtually indistinguishable; in addition, the accuracy results of both simulations are almost identical to the results obtained with the CAM3.5.41 version

of the NCAR Finite Volume (FV) dynamical core at the resolution 1° by 1° with 26 hybrid levels, as described in Jablonowski et al. (2008). Although we have used a relatively low resolution of H64 which is comparable to T63 of a spectral model, the results are strikingly similar to the solutions with the $1^\circ \times 1^\circ$ NCAR CAM-FV core, both in phase and amplitude.

2) Jablonowski-Williamson balanced initial state test

In order to estimate the accuracy and stability of the dynamical core, we conduct the Jablonowski-Williamson balanced initial state test introduced by Jablonowski and Williamson (2006). We initialize the model following Jablonowski and Williamson (2006a and b). Using the balanced initial fields, the simulation results should maintain the initial state perfectly for a sufficient amount of time. Since the initial state of this test is the true solution, we can compute error norms. We evaluate the error by using the relative L_2 error defined by

$$\|q_{simulation}\|_{L_2} = \sqrt{\frac{\int_{\Omega} (q_{exact} - q_{simulation})^2 d\Omega}{\int_{\Omega} q_{exact}^2 d\Omega}},$$

where $q_{simulation}$ represents the computed state variables and q_{exact} the exact (i.e., initial condition) values.

Figure 4 shows the normalized surface pressure L_2 error norms for the CG and DG simulations with $H = 128$ ($n_H = 16$ and $N = 8$) horizontal resolution and 26 vertical levels (Nlev=26). The L_2 error norms of the two simulations are visually identical, in which the error oscillates but remains bounded. These results (including the value of the L_2 error) compare well against those of the NSEAM model presented in GR04. The bounded error confirms that the initial balanced state is properly maintained. In practice though, the initial state degrades over time. After 20-days, the zonal wind fields for the CG and DG simulations show a somewhat distorted distribution with an increasing zonally asymmetric pattern (Fig.

5). Initially the maximum of the zonal winds at the lowest level are about 9.4 m/s in mid-latitude, but after 20-days the maximum difference of the zonal wind is up to about 0.02 m/s showing the zonal asymmetry. Although the error distribution is different between the CG and DG simulations in detail, these have a wavenumber 4 structure which arise from the cubed-sphere grid. The wavenumber 4 signals grow over time and lead eventually to a breakdown of the balanced state. However, higher resolutions delay the growth of the signals as the truncation error associated with the spatial discretization decreases. Actually, at $H = 192$ ($n_H = 16$ and $N = 12$) horizontal resolution this error virtually disappears for 20-day simulations (Fig. 6).

3) Jablonowski-Williamson baroclinic instability test

The baroclinic instability test case starts from the balanced initial fields, which is described above, with a perturbation in the initial zonal velocity. The baroclinic wave is induced by the small perturbation in the initial zonal wind. Here a Gaussian profile is used for the zonal wind perturbation, which is centered at $(\lambda_c, \varphi_c) = \left(\frac{\pi}{9}, \frac{2\pi}{9}\right)$ pointing to the location $(20^\circ\text{E}, 40^\circ\text{N})$. This perturbation is given by

$$u_{\text{perturbation}}(\lambda, \varphi, \sigma) = \exp\left[-\left(\frac{r}{R}\right)^2\right],$$

where

$$r = a \arccos\left[\sin \varphi_c \sin \varphi + \cos \varphi_c \cos \varphi \cos(\lambda - \lambda_c)\right],$$

and $R = a / 10$ is the perturbation radius (Jablonowski and Williamson 2006a and b).

Since the baroclinic wave test case does not have an analytic solution, we compare our results to the solutions from Jablonowski and Williamson (2006a) and the NSEAM model in

328 GR04. We show the surface pressure, 850 hPa temperature, and 850 hPa relative vorticity at
 329 day 9 for the CG and DG simulations with the resolution of $H = 80$ ($n_H = 16$ and
 330 $N = 5$) and 26 vertical levels (Nlev=26) in Fig. 7 which can be compared with the solutions
 331 of the National Center for Atmospheric Research's Community Atmosphere Model version 3
 332 (NCAR CAM3) Eulerian dynamical core at T85 resolution and finite volume core at 1° by
 333 1.25° from Jablonowski and Williamson (2006a). The CG and DG simulations in Fig. 7 are
 334 visually very similar to those reported in Jablonowski and Williamson with regard to the
 335 structure in the fields and the extrema for the surface pressure; in addition, the CG and DG
 336 results are almost identical to each other. Differences, however, can only be seen in the
 337 relative vorticity field at very small scales. In the CG simulation, the small-scale vorticity in
 338 the vicinity of the hook is depicted, and the maximum strength of the relative vorticity is
 339 larger than that of the DG simulation, which can be also seen in the results of a relatively
 340 higher resolution shown in Fig. 8. Figure 8 shows the same fields at day 9 as in Fig. 7 but for
 341 the higher resolution of $H = 160$ ($n_H = 32$ and $N = 5$) and 26 vertical levels (Nlev=26).
 342 In comparison with the results of the lower resolution of $H = 80$ ($n_H = 16$ and $N = 5$), it
 343 can be clearly seen that the numerical solutions of the two different resolutions are well
 344 converged in terms of the strength and structure in the surface pressure, temperature, and
 345 vorticity fields. It is noted that the vorticity fields in the higher resolution are characterized by
 346 the smallest scale in the vicinity of the hook, which is the same as in the lower resolution,
 347 which imply that the DG simulation is more diffusive than the CG simulation. It suggests that
 348 the diffusive property of the DG simulation is induced by the Rusanov numerical flux used in
 349 this study, because the only difference between the CG and DG formulations is the numerical
 350 flux and the fact that the DG solutions are allowed to contain jumps across element edges.
 351 However, this difference in the results suggests that it is the dissipation of the numerical flux

that is mainly responsible for the differences in the two simulations.

In general, the baroclinic wave grows observably around day 4. At day 7 the baroclinic wave evolves rapidly and by day 9 the wave train has intensified significantly (Jablonowski and Williamson 2006a). In order to examine the growth of the perturbation, an evolution of the minimum surface pressure is shown in Fig. 9 which we now compare with the results in G R04. The results of the CG and DG simulations with different resolutions are almost in agreement until day 10, at which point the simulations begin to show slight deviations from each other. The DG simulation with the lower resolution tends to simulate somewhat weak deepening. During the period between day 10 and 11 when wave breaking has set in, the remarkable weak deepening is shown in the DG simulation at the lower resolution. At day 14, the difference of the minimum surface pressure between the DG simulation at the lower resolution and the three other simulations is about 2 hPa.

4) Held-Suarez test

In order to estimate the capabilities of the model in simulating a realistic climate circulation without complex parameterizations, we conduct the Held-Suarez test. The Held-Suarez test ensures that a dynamical core produces a realistic zonal and time mean climate and synoptic eddies by using a simple Newtonian relaxation of the temperature field and a Rayleigh damping of low-level winds representing boundary-layer friction (Held and Suarez 1994). The Newtonian relaxation of the temperature is added as the diabatic forcing term to the thermodynamic equation, the fifth row of Eq. (1), and the Rayleigh damping is imposed as dissipation term in the momentum equation, the second to fourth rows of Eq. (1). The detailed specifications are adapted from Held and Suarez (1994). For this test we use a relatively low resolution of $H = 40$ ($n_H = 8$ and $N = 5$) with 25 vertical levels (Nlev=25) because this test case requires a relatively long model time simulation for 1200

days. In this paper, the integrations start from a stably stratified state at rest atmosphere, in which the lapse rate of temperature is 6.5 K/m and the surface temperature is 288 K. We use the simulation results from day 200 to day 1200 integrations sampled every 10-days.

Fig. 10 shows the time mean zonally averaged zonal wind and temperature for both the CG and DG simulations which can be easily compared to the results of other published papers. In comparison with the results of the spectral transform model in Held and Suarez (1994), both the CG and DG simulations show reasonable and comparable distributions, where the midlatitude jets at the upper troposphere near 250 hPa and the equatorial easterly flow in the lower and upper atmosphere are clearly visible in each hemisphere. Also temperature stratification is maintained realistically. The simulation results are comparable to that of GR04. There exist, however, differences between the results of the CG and DG simulations mainly in the strength of the westerly flow and the temperature structure in the upper atmosphere. DG simulates broader upper-level jet streams than CG that strengthen with altitude. Also in the temperature field, the DG simulation shows warmer air in the equatorial upper atmosphere. The difference is shown clearly in Fig. 11 where we plot the time mean zonally averaged eddy heat flux of the CG and DG simulations. There are two maxima at mid-latitude in the lower and upper atmosphere indicating transportations of heat in the poleward direction, of which the distributions in the CG and DG simulations are in good agreement with previous studies, for example, Held and Suarez (1994), Lin (2004) and Wan et al. (2008). However, in comparison of the strength and horizontal gradient of the eddy heat flux between both simulations, CG simulates a stronger eddy motion than DG.

6. Summary and Conclusions

We have proposed a hydrostatic dynamical solver using both the continuous Galerkin

(CG) and discontinuous Galerkin (DG) methods. It is solved on a cubed-sphere grid in 3D Cartesian coordinates although in principle any quadrilateral-based grid could be used. The CG and DG horizontal discretization employs a high-order nodal (Lagrange) basis function based on quadrilateral elements and GLL quadrature points which compose the common machinery. However, the DG method use fluxes along the boundaries of the elements which are approximated by the Rusanov method. In the vertical direction, a conservative flux-form finite-difference method is employed for coupling the dynamics with existing physics packages easily; we hope to report progresses on this specific topic in the future. A third-order strong stability preserving Runge-Kutta scheme was used for time integration although other time-integrators (including semi-implicit methods) could also be used.

In this paper, we show simulations of the model using four baroclinic test cases including: the Rossby-Haurwitz wave, balanced initial state, baroclinic instability, and Held-Suarez test cases. All cases, except for the Jablonowski-Williamson balanced initial state test case, do not have analytic solutions. Therefore, we compare our results to the results of test cases run by a vast community. Through our comparison of the CG and DG simulations, we show that for the baroclinic instability test and Held-Suarez test cases, the DG simulation tends to simulate somewhat weaker small-scale features, such as the minimum surface pressure perturbation and eddy heat flux, than the CG method. This could be due to the intrinsic diffusion of the Rusanov numerical flux scheme used for the horizontal discretization of the DG method, which is the only difference between the CG and DG formulations. One of the valuable contributions of this model is that we can use it to study the effects of using different horizontal discretizations since we use the exact same model with the same finite difference method in the vertical and time-integration methods but use either CG or DG in the horizontal. The discrete operators in the horizontal use the exact same numerical machinery and so the results shown here isolate the differences offered by the CG

and DG methods. However, for the other two test cases (Rossby-Haurwitz wave and balanced initial state tests), the results of the CG and DG simulations are virtually indistinguishable. Furthermore, the numerical results obtained for all four test cases show that the present dynamical core can produce numerical solutions of good quality comparable to other models. The results confirm that the CG and DG methods combined with the finite difference method in the vertical direction offer a viable strategy for atmospheric modeling. To our knowledge, we present the first results for a DG model for long-time simulations represented by the Held-Suarez test case. The importance of this result is that this confirms the stability of the DG method for long-time simulations in hydrostatic atmospheric dynamics. In order to make the model efficient and competitive with operational models, we need a semi-implicit time integration method which, although requires some additional machinery to be added, does not pose any theoretical barriers since such algorithms have already been designed by one of the authors in previous papers (Giraldo 2005, Giraldo et al. 2013).

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Figure Captions

FIG. 1. The cubed-sphere grid for (a) the $H = 3$ ($n_H = 3$ and $N = 1$), (b) the $H = 15$ ($n_H = 3$ and $N = 5$), and (c) the $H = 35$ ($n_H = 5$ and $N = 7$) horizontal resolutions.

FIG. 2. Numerical results for the CG simulation on the resolution of the $H = 64$ ($n_H = 8$ and $N = 8$) with 26 vertical levels: Top row: 850 hPa zonal wind and meridional wind, bottom row: surface pressure and 850 hPa temperature.

FIG. 3. As in Fig. 2 but for the DG simulation.

FIG. 4. L2 error norm of surface pressure in Pa for the CG and DG simulations at the $H = 128$ ($n_H = 16$ and $N = 8$) horizontal resolution and 26 vertical levels.

FIG. 5. Distribution of zonal wind difference at the lowest model level between day 20 and day 0 for the (top) CG and (bottom) DG simulations at the $H = 128$ ($n_H = 16$ and $N = 8$) horizontal resolution and 26 vertical levels.

FIG. 6. As in Fig. 5 but for the $H = 192$ ($n_H = 16$ and $N = 12$) horizontal resolution.

FIG. 7. Baroclinic wave at day 9 with the (left) CG and (right) DG simulations with the resolution of the $H = 80$ ($n_H = 16$ and $N = 5$) horizontal resolution and 26 vertical

levels: (upper row) surface pressure, (middle row) 850 hPa temperature, and (bottom row) 850 hPa relative vorticity at days (left) 7 and (right) 9.

FIG. 8. As in Fig. 7 but for the $H = 160$ ($n_H = 32$ and $N = 5$).

FIG. 9. The minimum surface pressure (hPa) as a function of days for the CG and DG simulations with the lower resolution of the $H = 80$ ($n_H = 16$ and $N = 5$) and the higher resolution of the $H = 160$ ($n_H = 32$ and $N = 5$).

FIG. 10. The (left) mean zonally averaged zonal velocity (m/s) and (right) mean zonally averaged temperature (K) for the (upper row) CG and (bottom row) DG simulations with the resolution of the $H = 40$ ($n_H = 8$ and $N = 5$) and 25 vertical levels (Nlev=25). These are calculated over the last 1000 days of a 1200-day integration.

FIG. 11. The mean zonally averaged eddy heat flux for the (left) CG and (right) DG simulation with the resolution of the $H = 40$ ($n_H = 8$ and $N = 5$).

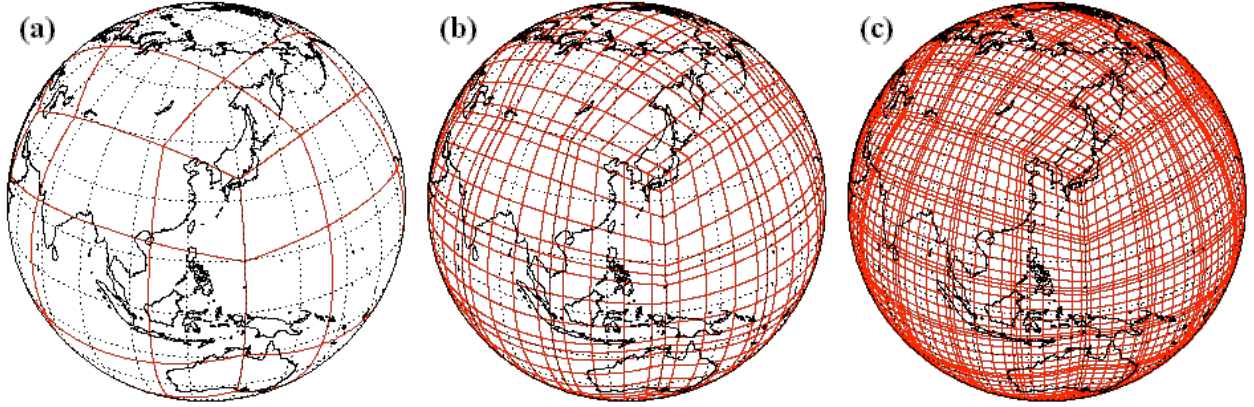


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Snapshots of the Rossby-Haurwitz wave at day 15
simulated with KIAPS-H_CG.Np08xNe08L26

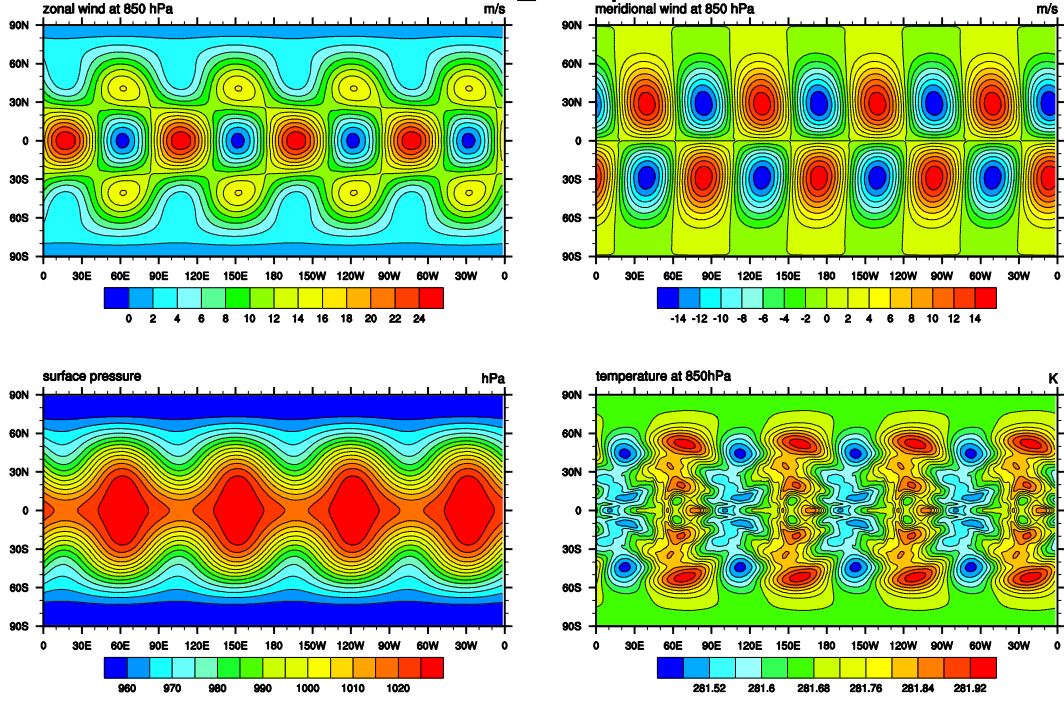
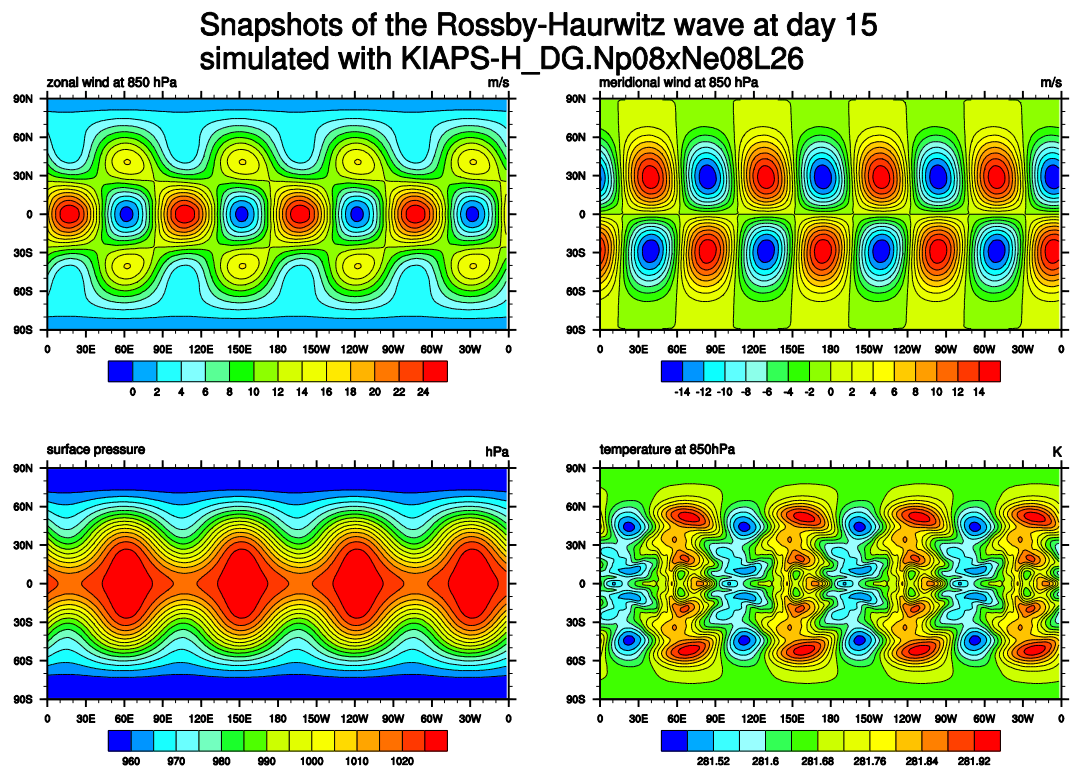


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FIG. 3. As in Fig. 2 but for the DG simulation.

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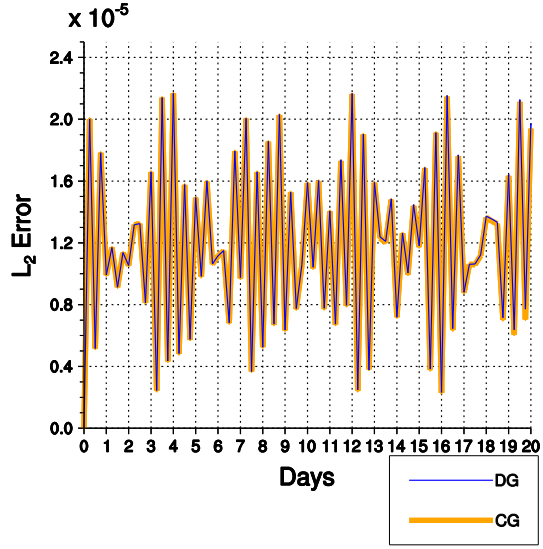


FIG. 4. L2 error norm of surface pressure in Pa for the CG and DG simulations at the $H = 128$ ($n_H = 16$ and $N = 8$) horizontal resolution and 26 vertical levels.

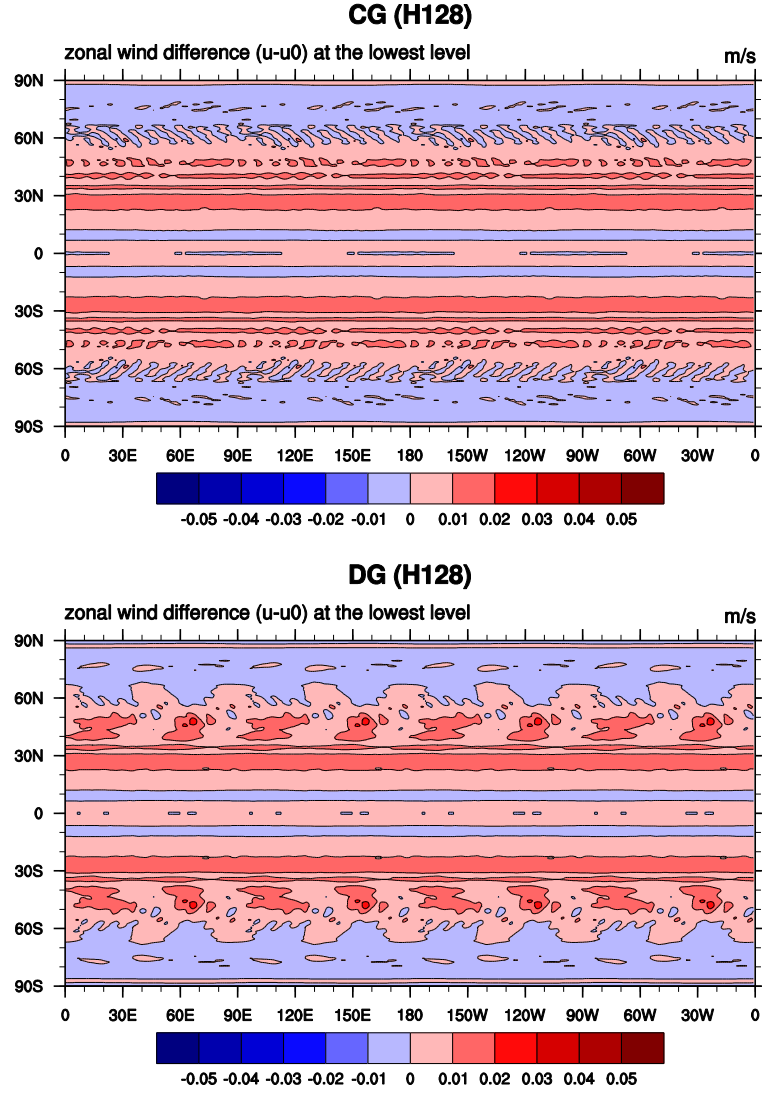


FIG. 5. Distribution of zonal wind difference at the lowest model level between day 20 and day 0 for the (top) CG and (bottom) DG simulations at the $H = 128$ ($n_H = 16$ and $N = 8$) horizontal resolution and 26 vertical levels.

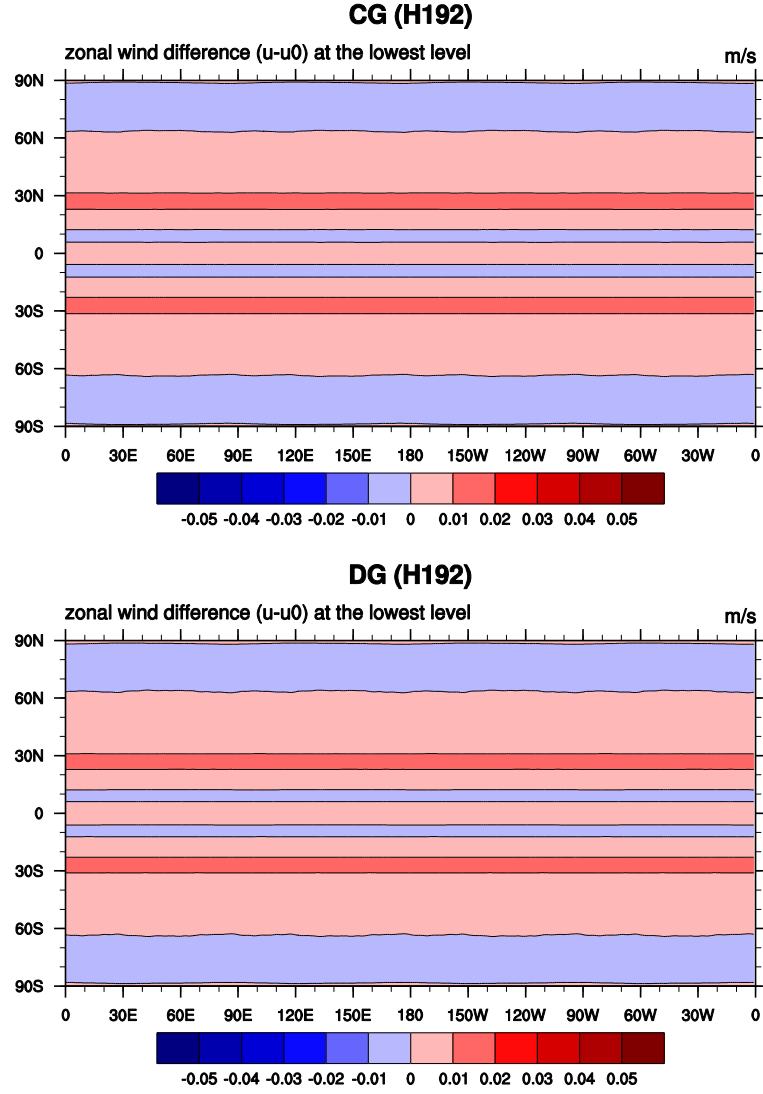


FIG. 6. As in Fig. 5 but for the $H = 192$ ($n_H = 16$ and $N = 12$) horizontal resolution.

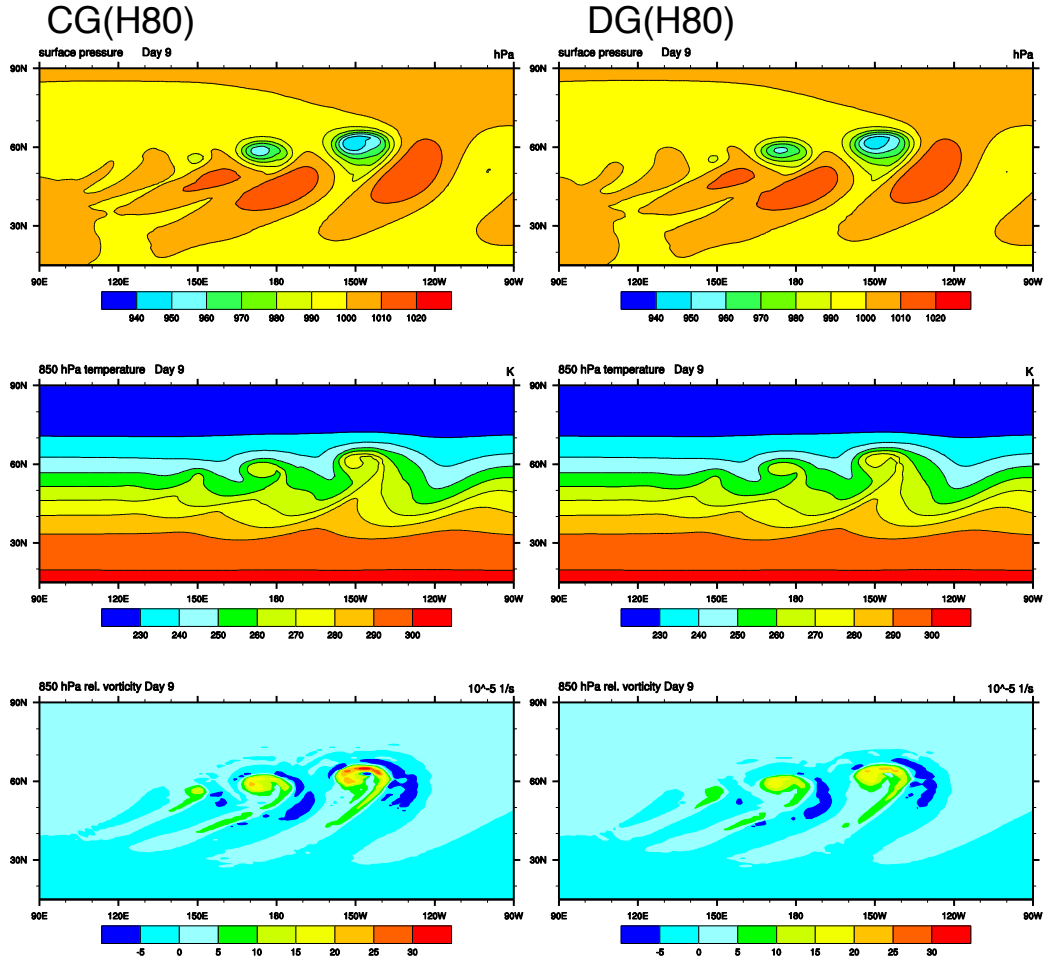


FIG. 7. Baroclinic wave at day 9 with the (left) CG and (right) DG simulations with the resolution of the $H = 80$ ($n_H = 16$ and $N = 5$) horizontal resolution and 26 vertical levels: (upper row) surface pressure, (middle row) 850 hPa temperature, and (bottom row) 850 hPa relative vorticity at days (left) 7 and (right) 9.

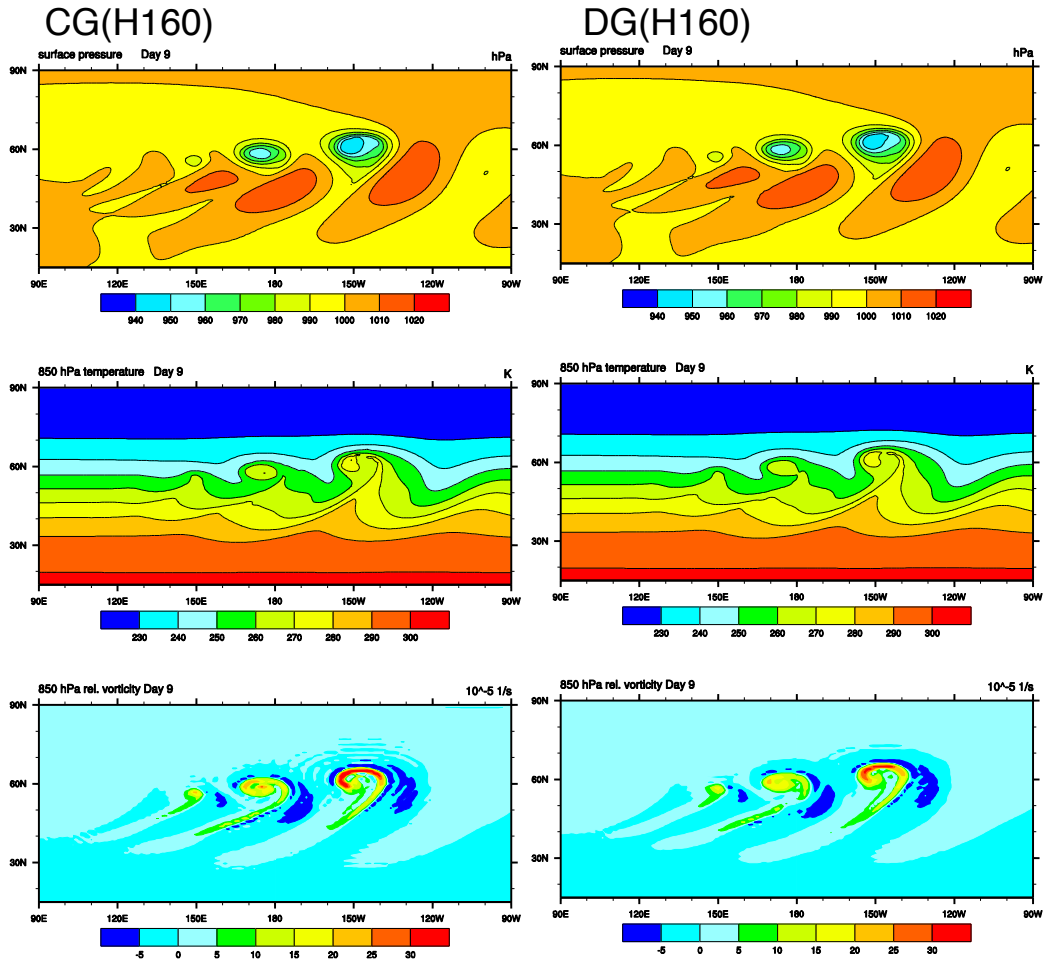


FIG. 8. As in Fig. 7 but for the $H = 160$ ($n_H = 32$ and $N = 5$).

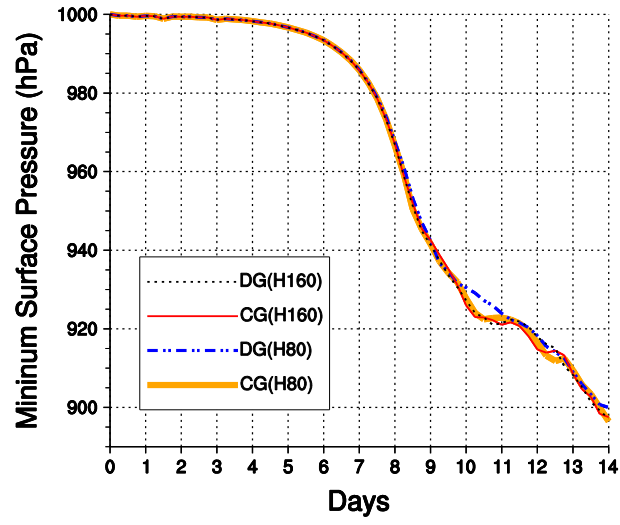


FIG. 9. The minimum surface pressure (hPa) as a function of days for the CG and DG simulations with the lower resolution of the $H = 80$ ($n_H = 16$ and $N = 5$) and the higher resolution of the $H = 160$ ($n_H = 32$ and $N = 5$).

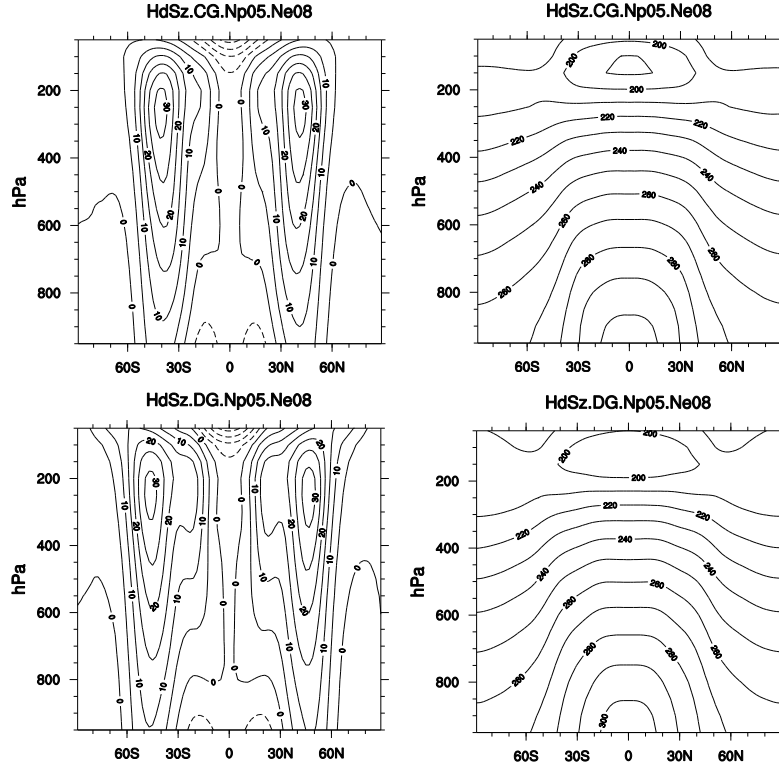


FIG. 10. The (left) mean zonally averaged zonal velocity (m/s) and (right) mean zonally averaged temperature (K) for the (upper row) CG and (bottom row) DG simulations with the resolution of the $H = 40$ ($n_H = 8$ and $N = 5$) and 25 vertical levels (Nlev=25). These are calculated over the last 1000 days of a 1200-day integration.

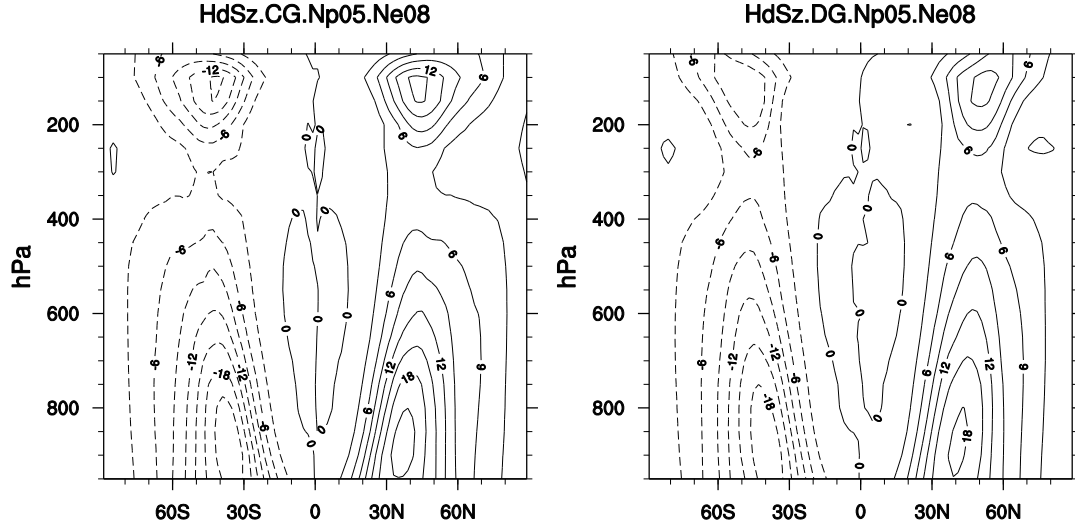


FIG. 11. The mean zonally averaged eddy heat flux for the (left) CG and (right) DG simulation with the resolution of the $H = 40$ ($n_H = 8$ and $N = 5$).